

SPP DISIS-2020-001 AFS STUDY REPORT

INTRODUCTION

Associated Electric Cooperative Inc. (AECI), through coordination with the Southwest Power Pool (SPP), has performed the analysis for generator interconnection requests (GIRs) within the DISIS-2020-001 Study Cycle (the “Study Cycle”) for an Affected System Study (AFS) evaluation on the AECI transmission system (the “Study”). The restudy has been conducted to include the withdrawal of fifteen (15) SPP Study Cycle requests as listed in Table 1 below.

Table 1: Withdrawn Study Cycle Requests

Project#	CA	Capacity (MW)	Fuel Type	POI
GEN-2020-001	BEPC	200	Solar	Sidney 345 kV Substation
GEN-2020-009	AEP	300	Solar	Lawton East Side to Oklaunion 345 kV Line
GEN-2020-016	WFEC	202	Wind	Snyder SW to Cache 138 kV Line
GEN-2020-023	OGE	202	Battery Storage	Woodring 345 kV Substation
GEN-2020-036	OPPD	303	Solar	Substation 3740; 345 kV Substation
GEN-2020-052	WERE	251	Wind	Neosho to Delaware 345 kV Line
GEN-2020-059	SPS	250	Solar	Tuco to Yoakum to Hobbs 345 kV Line
GEN-2020-062	SPS	256	Solar	OASIS 230 kV Substation
GEN-2020-070	SUNC	255	Solar	Postrock to Axtell 345 kV Line
GEN-2020-071	WERE	252	Wind	Swissvale to Morris 230 kV Line
GEN-2020-075	AEP	200	Battery Storage	Cimmarron to Lawton 345 kV Line
GEN-2020-076	WERE	200	Battery Storage	Benton to Wolf Creek 345 kV Line
GEN-2020-077	NPPD	151	Battery Storage	North Hebron to Fairbury 115 kV Line
GEN-2020-086	WERE	500	Solar	Benton to Wolf Creek 345 kV Line
GEN-2020-089	WERE	104	Solar	Dakota 161 kV Substation

The full list of Study Cycle requests included in the Study are listed in Table 2 below.

Table 2: Study Cycle Requests Evaluated

Project#	CA	Capacity (MW)	Fuel Type	POI
ASGI-2020-001	KCPL	45	Solar	Waverly 69 kV Substation (Mt. Leonard)
ASGI-2020-003	KCPL	45	Solar	Coroltown 161 kV Substation (Bogard)
GEN-2020-002	OPPD	81	Solar	6846 69 kV Substation
GEN-2020-007	KCPL	650	Hybrid	Every La Cygne to Wolf Creek 345 kV Line
GEN-2020-008	SPS	250	Hybrid	Corporation Carpenter 345 kV Substation
GEN-2020-010	WFEC	140	Hybrid	Seiling to Taloga 138 kV Line

Project#	CA	Capacity (MW)	Fuel Type	POI
GEN-2020-011	NPPD	320	Hybrid	Axtell 345 kV Substation
GEN-2020-012	AEP	113	Hybrid	Snyder to Altus Jct. 138 kV Line
GEN-2020-013	NPPD	215	Hybrid	Orleans to Holdrege 115 kV Line
GEN-2020-020	AEP	202	Hybrid	Northwest Texarkana to Valliant 345 kV Line
GEN-2020-021	BEPC	235	Wind	LeLand Olds to Chapelle Creek 345 kV Line
GEN-2020-025	OPPD	255	Thermal	Substation 1363; 161 kV Substation
GEN-2020-028	OPPD	255	Thermal	Substation 1363; 161 kV Substation
GEN-2020-031	OPPD	303	Thermal	Substation 1363; 161 kV Substation
GEN-2020-038	OPPD	303	Thermal	Substation 3740; 345 kV Substation
GEN-2020-054	AEP	298	Solar	Lydia 345 kV Substation
GEN-2020-057	WERE	425	Battery Storage	Atlantic 345 kV Substation
GEN-2020-058	KCPL	425	Solar	Atlantic 345 kV Substation
GEN-2020-060	SPS	200	Battery Storage	Lubbock East 230 kV Substation
GEN-2020-065	SPS	1003	Thermal	Hobbs to Andrews 345 kV Line
GEN-2020-067	SPS	353	Wind	Tuco to Yoakum 345 kV Line
GEN-2020-068	SPS	400	Solar	Tuco to Yoakum 345 kV Line
GEN-2020-072	GMO	150	Hybrid	Windsor to AEC Sedalia 161 kV Line
GEN-2020-073	KCPL	150	Hybrid	SE Ottawa to Pleasant Valley 161 kV Line
GEN-2020-074	AEP	200	Battery Storage	Lawton to Sunnyside 345 kV Line
GEN-2020-078	OPPD	100	Solar	Substation 1226 to Substation 1237 161 kV Line
GEN-2020-079	EDE	225	Hybrid	Riverton to Neosho 161 kV Line
GEN-2020-081	AEP	200	Battery Storage	Tenaska Switching 345 kV Substation
GEN-2020-084	OPPD	350	Solar	Raun to Fort Calhoun 345 kV Line
GEN-2020-085	AEP	500	Solar	Lawton to Sunnyside 345 kV Line
GEN-2020-087	AEP	500	Solar	Cimarron to Lawton 345 kV Line
GEN-2020-088	EDE	150	Solar	La Russell 161 kV Substation
GEN-2020-090 ¹	WERE	204	Battery Storage	Wolf Creek to Blackberry 345 kV Line
GEN-2020-091	BEPC	150	Solar	Patent Gate 345 kV Substation
GEN-2020-092	AEP	100	Solar	Pryor Junction to Midwest Carbide 138 kV Line
GEN-2020-094	OPPD	250	Solar	Neb. City to 103rd & Rokeby 345 kV Line
GEN-2020-064	EDE	64	Thermal	4544 Stateline CC 161 kV Substation

¹ GEN-2020-090's POI was not studied at the Wolf Creek to Blackberry 345 kV line due to this change occurring after the study was started. The POI was studied on the Neosho to Blackberry 345 kV line. This did not materially impact the study results.

INPUTS AND ASSUMPTIONS

Each of the SERC member transmission planners is responsible for submitting system modeling data to SERC for development of the power flow models. Power flow analysis utilized the latest Long-Term Working Group (LTWG) models as developed by SERC Reliability Corporation (SERC). Each of the power flow models for the steady state analysis was modified to include appropriate higher-queued generation interconnection requests. Modeling parameters from the SPP DISIS-2020-001 steady state models were referenced for each of the Study Cycle requests.

Full details of the inputs and assumptions are provided in Appendix A.

METHODOLOGY

Steady state analysis was performed to confirm the reliability impacts on the AECI system under a variety of system conditions and outages. AECI's transmission system must be capable of operating within the applicable normal ratings, emergency ratings, and voltage limits of AECI planning criteria. AECI is a member of SERC, one of eight Electric Reliability Organizations under the North American Electric Reliability Corporation (NERC). As a member of SERC, AECI develops its planning criteria consistent with NERC Reliability Planning Standards and the SERC planning criteria. The NERC TPL-001-5 Planning Standard Table 1 requires that, for normal and contingency conditions, line and equipment loading shall be within applicable thermal limits, voltage levels shall be maintained within applicable limits, all customer demands shall be supplied (except as noted), and stability of the network shall be maintained.

In evaluating the impacts of the Study Cycle requests, the following thermal and voltage limits were applied to the analysis for P0 or normal system conditions:

- Thermal Limits within Applicable Rating – Applicable Rating shall be defined as the Normal Rating. The thermal limit shall be 100% of Rating A.
- Voltage Limits within Applicable Rating – Applicable Rating shall have the meaning of Nominal Voltage. Voltage limits shall be set at plus or minus five percent (+/- 5%), 0.95 p.u. - 1.05 p.u. for systems operating at 60 kV or above on load serving buses.

The following thermal and voltage limits were applied to the analysis for contingency conditions under P1 and P2EHV planning events:

- Thermal Limits within Applicable Rating – Applicable Rating shall be defined as the Emergency Rating. The thermal limit shall be 100% of Rating B.
- Voltage Limits within Applicable Rating – Applicable Rating shall have the meaning of Nominal Voltage. Voltage limits shall be set at plus five percent to minus ten percent (+5%/-10%), 0.90 p.u. – 1.05 p.u. for systems operating at 60 kV or above on load serving buses.

In order for the Study Cycle requests to have a negative impact (i.e. criteria violation) on the system, the Study Cycle must cause a three percent (3%) or greater increase in flow on an overloaded facility based upon the rating of the facility. In order for the Project to have a negative voltage impact on the system, the Project must cause a voltage violation and have a two percent (2%) or greater change in the voltage.

System upgrades are required for constraints resulting from the addition of the Study Cycle requests under P0, P1, P2.1, P2.2 (EHV only), and P2.3 (EHV only) system conditions. For the purpose of this study, P2.1

events are included as part of the P1 contingency file. As such, these events will be denoted as a P1 event in the results. All improvements were developed and studied in coordination with AECI.

AECI will perform an annual limited operations study which will indicate seasonal operating limits for SPP/MISO/AECI generation interconnection requests that will reach commercial operation in the 12-month horizon but whose AECI network upgrades have not yet been energized.

STEADY STATE ANALYSIS RESULTS

Steady state analysis results showed three (3) constraints reported on the AECI transmission system, as shown in Table 3, which are attributed to the Study Cycle requests. Transmission upgrades were evaluated to mitigate the impacts reported from the analysis as a result of the Study Cycle requests. Simulations were performed on each of the scenarios with the identified network upgrade and contingent network upgrades included.

The upgrades shown in Table 7 were evaluated in order to mitigate the reported steady state constraints for the Study Cycle requests; results from the simulations found that the network upgrades were able to mitigate the reported overload conditions as shown in Table 3.

Table 3: Steady State Constraints for the Study Cycle Requests with Upgrades

Constraint ID	Event	Monitored Facility	Contingency	Season	Base Loading	Project Loading	Upgrade Loading
NU01	P1	300520 2REFORM 69.000 300626 2CHAMOI 69.000 1	OPEN LINE FROM BUS 300060 [5BIGSPG 161.00] TO BUS 300067 [5CHAMOI 161.00] CKT 1	28W	107.9	112.8	63.7
				33W	109.0	113.7	64.2
	P2EHV		OPEN BRANCH FROM BUS 345230 [7MONTGMRY 345.00] TO BUS 41454 [J1145 POI 345.00] CKT 2 OPEN BRANCH FROM BUS 41454 [J1145 POI 345.00] TO BUS 300044 [7MCCRED 345.00] CKT 1	28W	94.5	100.8	56.9
NU02	P1	300534 2LINCLN 69.000 300558 2MTHULD 69.000 1	OPEN LINE FROM BUS 300541 [2SEDALI 69.000] TO BUS 300545 [2SYLVAN 69.000] CKT 1	33W	89.1	100.2	41.3
NU03	P1	301370 5TURKEYCRK 161.00 301401 2TURKEYCRK 69.000 1	OPEN BRANCH FROM BUS 300034 [5EDMONS 161.00] TO BUS 301402 [5LOSTVALY 161.00] CKT 1	28W	96.9	101.8	96.1 ²
				33W	97.7	102.8	96.4 ²

Table 3 shows stressed modeling conditions in which the Base Loading represents models built with higher queue generation requests in service, but without network upgrades tagged to those higher queue requests. Multiple iterations of solutions, which can include applicable higher queued network upgrades, were tested to alleviate both the Base Loading and the additional loading contributed by the Study Cycle (Project Loading).

² Upgrade loading reflects adjustment of transformer taps as mitigation.

CONTINGENT FACILITY RESULTS

Seven (7) facilities were reported as Contingent Facilities with the addition of the Study Cycle requests, as shown in Table 4. Contingent Facilities are those facilities identified that are the responsibility of higher-queued generators or are included in the Transmission Provider's transmission expansion plan and that if not included in the Study may otherwise be the responsibility of the Study Cycle requests as necessary to interconnect to the transmission system.

The transmission upgrades for the Contingent Facilities were evaluated in order to confirm that the planned system adjustments were sufficient to mitigate the overload seen for the addition of the Study Cycle requests. Simulations were performed on each of the scenarios with the identified network upgrade and contingent network upgrades included. The upgrades shown in Table 6 were evaluated in order to mitigate the reported constraints as listed in Table 4 below.

Table 4: Steady State Contingent Constraints for the Study Cycle Requests with Upgrades

Constraint ID	Event	Monitored Facility	Season	Base Loading	Project Loading	Upgrade Loading	Contingent Generator(s)
CF01	P1	300115 5STFRANB2 161.00 338202 5JIM HILL% 161.00 1	33S	101.4	104.7	37.4	MISO DPP-2019
	P2EHV			101.4	104.7	37.4	
CF02	P1	300327 2ELM 69.000 300336 2HOLDEN 69.000 1	28S	98.5	101.8	75.1	MISO DPP-2019
CF03	P1	300069 5CHOTEAU1 161.00 512648 MAID 5 161.00 1	28H	90.9	101.2	57.4	SPP DISIS-2017-002
			28S	91.2	100.9	57.3	
			33S	91.3	101.0	57.3	
CF04	P2EHV	300045 7MORGAN 345.00 301622 5MORGANXF1 161.00 1	28S	94.7	101.6	60.7	SPP DISIS-2018-001
			28W	105.9	111.3	66.7	

Constraint ID	Event	Monitored Facility						Season	Base Loading	Project Loading	Upgrade Loading	Contingent Generator(s)
								33S	95.5	101.8	60.8	
								33W	105.3	111.1	66.5	
CF05	P1	300530 2GEOGT2 69.000 300541 2SEDALI 69.000 1						28S	98.7	128.2	86.3	GI-091
								33S	97.2	127.0	85.5	
CF06	P1	300541 2SEDALI 69.000 300545 2SYLVAN 69.000 1						28W	102.6	114.8	63.5	GI-091
								33W	106.3	118.3	65.5	
CF07	P1	300101 5MORGAN 161.00 505498 STOCKTN5 161.00 1						28W	86.6	100.8	64.6	AECI
	P2EHV							28W	89.5	105.8	67.8	
								33W	87.5	104.1	66.8	

NEIGHBORING SYSTEM RESULTS

No facilities were reported on the AECI ties with the addition of the Study Cycle requests.

NETWORK UPGRADES

Transmission upgrades were evaluated to mitigate the impacts reported from the analyses as a result of the Study Cycle projects. The upgrades shown in Table 5 were evaluated in order to mitigate the reported steady state constraints for the Study Cycle as listed in Table 3.

Table 5: Network Upgrades for the Study Cycle Constraints

Constraint ID	Monitored Facility	Network Upgrade
NU00A	Sedalia 161 kV Substation Modifications	Modification to Sedalia 161 kV substation required for GEN-2020-072 to interconnect on Windsor-Sedalia 161 kV line
NU00B	Blackberry 345 kV Substation Modifications	Modification to Blackberry 345 kV substation required for GEN-2020-090 to interconnect on Wolf Creek-Blackberry 345 kV line
NU01	300520 2REFORM 69.000 300626 2CHAMOI 69.000 1	CT tap adjustments are able to mitigate overload; no upgrade evaluated.
NU02	300534 2LINCLN 69.000 300558 2MTHULD 69.000 1	Upgrade bushing CTs (via breaker upgrade) on Lincoln- Mt. Hulda 69 kV line (at Lincoln) with 1200 amp equipment. Upgrade jumpers on Lincoln-Mt. Hulda 69 kV line (at Mt. Hulda) to 795 ACSR.
NU03	301370 5TURKEYCRK 161.00 301401 2TURKEYCRK 69.000 1	Tap adjustments able to mitigate overload; no upgrade evaluated.

The upgrades shown in Table 6 were evaluated in order to mitigate the reported steady state contingent constraints for the Study Cycle requests as listed in Table 4.

Table 6: Network Upgrades for the Study Cycle Contingent Constraints

Constraint ID	Monitored Facility	Network Upgrade
-	300651 2LAMR 69.000 300794 5LAMAR 161.00 1	Contingent on MISO Tranche 1 Build new 345 kV line from Orient 345 kV substation (Ameren) to Fairport 345 kV substation (Ameren/AECI). Build new 345 kV line from Fairport 345 kV substation to Zachary 345 kV substation (Ameren). Build new 345 kV line from Thomas Hill 345 kV substation (AECI) to Zachary 345 kV substation. Build new 345 kV line from Zachary 345 kV substation to Maywood 345 kV substation (Ameren). Build new 345 kV line from Meredosia 345 kV substation (Ameren) to Maywood 345 kV substation. Tap the existing 161 kV line from Adair 161 kV substation to Appanoose 161 kV substation with the Zachary 161 kV substation. Install a second Lamar 161/69 kV Xfmer rated at 84 MVA Summer, 95 MVA Winter unit. Rebuild 69 kV 6.31 mile long line from Coffman Bend to J-7 to 795 ACSR rated at 100C. Rebuild 69 kV 4.70 mile long line from Coffman Bend to Knobby to 795 ACSR rated at 100C. Rebuild 69 kV 12.1 mile long line from Knobby to Turkey Creek to 795 ACSR rated at 100 C.
-	300772 2COFMAN 69.000 300779 2J&7 69.000 1	
-	300772 2COFMAN 69.000 300780 2KNOBBY 69.000 1	
-	300780 2KNOBBY 69.000 301401 2TURKEYCRK 69.000 1	
-	301201 2DONIPH 69.000 505440 DONIPHNS 161.00 1	
-	300123 5WPLAINW 161.00 301123 2WSTPL3 69.000 1	
-	300505 2STURGN 69.000 300508 5STURGN 161.00 3	

Constraint ID	Monitored Facility	Network Upgrade
-	300505 2STURGN 69.000 300508 5STURGN 161.00 4	
CF01	300115 5STFRANB2 161.00 338202 5JIM HILL% 161.00 1	Contingent on MISO DPP-2019: Rebuild 9.9 mile-long St. Francis to Jim Hill 161 kV line to 1192 ACSS at 250C. Replace jumpers at St. Francis with 1192 ACSS at 250C. Replace disconnect switches at St. Francis 161 kV bus on Jim Hill line with 4000A switches.
CF02	300327 2ELM 69.000 300336 2HOLDEN 69.000 1	Contingent on MISO DPP-2019: Rebuild 3.1 mile 336 ACSR segment of Elm to Holden 69 kV line. Utilize 556 ACSR at 100C for 69 kV circuit.
CF03	300069 5CHOTEAU1 161.00 512648 MAID 5 161.00 1	Contingent on SPP DISIS-2017-002: Construct a new 161 kV switchyard ("Patrol Road") on the Maid to Gerald 161 kV line ~1 mile from Maid. Construct a new 0.8 mile-long 161 kV line from Chouteau to Patrol Road switchyard: - Construct as double bundle 1590 ACSR conductor, rated at 100C. - Series reactor installed on line to match impedance reactor on existing Chouteau-Maid line. - Reactor Impedance: 5 ohms, 12.263 mH. - All terminal equipment/reactors rated for 4,000 amps. At Chouteau Substation: - Add a 4,000 amp 161 kV breaker and associated equipment to the existing Chouteau to Maid line. - Add a new 161 kV terminal and associated equipment for the new 161 kV line to Patrol Road. At Chouteau West Yard: - Upgrade East to West bus from 5" to 6" bus.
CF04	300045 7MORGAN 345.00 301622 5MORGANXF1 161.00 1	Contingent on SPP DISIS-2018-001: Replace the Morgan 345/161 kV transformer with a unit rated 712 MVA Summer and 811 MVA Winter. Upgrade 161 kV breaker switchers and relay limits to 3,000 amps.
CF05	300530 2GEOGT2 69.000 300541 2SEDALI 69.000 1	Contingent on GI-091: Upgrade bushing CTs (via breaker upgrade), breaker switchers on Georgetown to Sedalia 69 kV line (at Sedalia) to 1200 amp rating.
CF06	300541 2SEDALI 69.000 300545 2SYLVAN 69.000 1	Contingent on GI-091: Upgrade bushing CTs (via breaker upgrade), breaker switchers on Sylvan to Sedalia 69 kV line (at Sedalia) to 1200 amp rating.
CF07	300101 5MORGAN 161.00 505498 STOCKTN5 161.00 1	Contingent on AECI: Upgrade Morgan to Stockton 161 kV line, less than 1 mile lake crossing, to 1192 ACSR at 100C. Upgraded line length is 17.3 miles.

No upgrades were evaluated for the neighboring system constraints.

AECI developed non-binding, good faith estimates of the timing and cost estimates for upgrades needed as a result of the addition of the Study Cycle requests as shown in Table 7.

Table 7: Network Upgrade Costs

ID	Option/Description	Estimated Cost	Estimated Lead Time ³
NU00A ⁴	Modification to Sedalia 161 kV station required for GEN-2020-072 to interconnect on Windsor-Sedalia 161 kV line	\$250,000	30 months
NU00B ⁴	Modification to Blackberry 345 kV station required for GEN-2020-090 to interconnect on Wolf Creek-Blackberry 345 kV line	\$350,000	30 months
NU01	CT tap adjustments are able to mitigate overload; no upgrade evaluated.	\$0	-
NU02	Upgrade bushing CTs (via breaker upgrade) on Lincoln to Mt. Hulda 69 kV line (at Lincoln) with 1200 Amp equipment. Upgrade jumpers on Lincoln to Mt. Hulda 69 kV line (at Mt. Hulda) to 795 ACSR.	\$650,000	36 months
NU03	Tap adjustments able to mitigate overload; no upgrade evaluated.	\$0	-
	Total Cost:	\$1,250,000	

Cost allocations for each of the impacted facilities are discussed in the Cost Allocation section below.

³ Estimated Lead Time is the estimated time to place a network upgrade in service once AECI has received Provision of Security equal to the total Estimated Cost of the Network Upgrade.

⁴ The Study Cycle request connects on a transmission line that terminates at an AECI owned station. This request is responsible for all costs associated with the work required to ready the AECI station for the newly interconnected Study Cycle request.

COST ALLOCATION

Network upgrade costs are allocated to each of the Study Cycle projects based on the worst MW impact⁵ each project had on the constraint and as described in the steps below:

1. Determine the MW impact each Study Cycle project had on each constraint using the size of each request in the season it was reported:

$$\text{Project X MW Impact on Constraint 1} = DFAX (X) * MW (X) = X1$$

$$\text{Project Y MW Impact on Constraint 1} = DFAX (Y) * MW (Y) = Y1$$

$$\text{Project Z MW Impact on Constraint 1} = DFAX (Z) * MW (Z) = Z1$$

2. Determine the maximum MW% impact each generator has as a percentage of the total Study Cycle impact on a given constraint.

$$X2 = \text{Project X MW impact \%} = \frac{X1}{\text{Total MW Impact of Study Cycle on Constraint}}$$

$$Y2 = \text{Project Y MW impact \%} = \frac{Y1}{\text{Total MW Impact of Study Cycle on Constraint}}$$

$$Z2 = \text{Project Z MW impact \%} = \frac{Z1}{\text{Total MW Impact of Study Cycle on Constraint}}$$

3. Apply three percent (3%) MW impact De Minimis Threshold: If a Study Cycle project MW% impact is less than 3% for a particular constraint then the project MW% impact is adjusted to 0 for that constraint and the Study Cycle project will not be allocated cost for that particular constraint.
4. Determine the cost allocated to each remaining Study Cycle project for each upgrade using the total cost of a given upgrade:

$$\text{Project X Upgrade 1 Cost Allocation (\$)} = \frac{\text{Network Upgrade 1 Cost (\$)} * X2}{X2 + Y2 + Z2}$$

The associated cost allocation of the network upgrades to each of the Study Cycle projects is shown below in Table 8. Further breakdown of costs is provided in Appendix B.

⁵ All negative MW impacts (helpers) were set to 0 MW impact.

Table 8: Network Upgrade Cost Allocation

Project	Cluster Group	POI	MW	Total Cost
ASGI-2020-001	03 CENTRAL	Waverly 69 kV Substation (Mt. Leonard)	45	\$42,400
ASGI-2020-003	03 CENTRAL	Coroltown 161 kV Substation (Bogard)	45	\$0
GEN-2020-002	02 NEBRASKA	6846 69 kV Substation	81	\$0
GEN-2020-007	03 CENTRAL	Evergy La Cygne to Wolf Creek 345 kV Line	650	\$100,709
GEN-2020-008	03 CENTRAL	Corporation Carpenter 345 kV Substation	250	\$0
GEN-2020-010	04 SOUTHEAST	Seiling to Taloga 138 kV Line	140	\$0
GEN-2020-011	02 NEBRASKA	Axtell 345 kV Substation	320	\$0
GEN-2020-012	04 SOUTHEAST	Snyder to Altus Jct. 138 kV Line	113	\$0
GEN-2020-013	02 NEBRASKA	Orleans to Holdrege 115 kV Line	215	\$0
GEN-2020-020	04 SOUTHEAST	Northwest Texarkana to Valliant 345 kV Line	202	\$0
GEN-2020-021	01 NORTH	LeLand Olds to Chapelle Creek 345 kV Line	235	\$0
GEN-2020-025	02 NEBRASKA	Substation 1363; 161 kV Substation	255	\$0
GEN-2020-028	02 NEBRASKA	Substation 1363; 161 kV Substation	255	\$0
GEN-2020-031	02 NEBRASKA	Substation 1363; 161 kV Substation	303	\$0
GEN-2020-038	02 NEBRASKA	Substation 3740; 345 kV Substation	303	\$0
GEN-2020-054	04 SOUTHEAST	Lydia 345 kV Substation	298	\$0
GEN-2020-057	03 CENTRAL	Atlantic 345 kV Substation	425	\$77,535
GEN-2020-058	03 CENTRAL	Atlantic 345 kV Substation	425	\$77,535
GEN-2020-060	05 SOUTHWEST	Lubbock East 230 kV Substation	200	\$0
GEN-2020-064	03 CENTRAL	4544 Stateline CC 161 kV Substation	64	\$0
GEN-2020-065	05 SOUTHWEST	Hobbs to Andrews 345 kV Line	1003	\$0
GEN-2020-067	05 SOUTHWEST	Tuco to Yoakum 345 kV Line	353	\$0
GEN-2020-068	05 SOUTHWEST	Tuco to Yoakum 345 kV Line	400	\$0
GEN-2020-072	03 CENTRAL	Windsor to AEC Sedalia 161 kV Line	150	\$571,023
GEN-2020-073	03 CENTRAL	SE Ottawa to Pleasant Valley 161 kV Line	150	\$30,799
GEN-2020-074	04 SOUTHEAST	Lawton to Sunnyside 345 kV Line	200	\$0
GEN-2020-078	02 NEBRASKA	Substation 1226 to Substation 1237 161 kV Line	100	\$0
GEN-2020-079	03 CENTRAL	Riverton to Neosho 161 kV Line	225	\$0
GEN-2020-081	04 SOUTHEAST	Tenaska Switching 345 kV Substation	200	\$0
GEN-2020-084	02 NEBRASKA	Raun to Fort Calhoun 345 kV Line	350	\$0
GEN-2020-085	04 SOUTHEAST	Lawton to Sunnyside 345 kV Line	500	\$0
GEN-2020-087	04 SOUTHEAST	Cimmarron to Lawton 345 kV Line	500	\$0
GEN-2020-088	03 CENTRAL	La Russell 161 kV Substation	150	\$0
GEN-2020-090	03 CENTRAL	Wolf Creek to Blackberry 345 kV Line	204	\$350,000
GEN-2020-091	01 NORTH	Patent Gate 345 kV Substation	150	\$0

Project	Cluster Group	POI	MW	Total Cost
GEN-2020-092	04 SOUTHEAST	Pryor Junction to Midwest Carbide 138 kV Line	100	\$0
GEN-2020-094	02 NEBRASKA	Neb. City to 103rd & Rokeby 345 kV Line	250	\$0
			Total Cost	\$1,250,000

VERSION HISTORY

Version Number and Date	Author	Change Description
V0 – 02/16/2024	AECI	Initial release
V1 – 08/13/2025	AECI	Re-study with the removal of 15 generators that withdrew from the SPP queue since the initial study.